

LOW COST SQUIB DRIVER FOR AIRBAG APPLICATION

RELATED PATENT APPLICATION

This application is related to US patent application docket number DS03-027, serial number _###/###,###_, filed concurrently, and assigned to the same assignee as the present invention. Title: "Squib Driver for Airbag Application"

BACKGROUND OF THE INVENTION

(1) Field of the Invention

The present invention relates in general to electronic circuits as used within Supplemental Inflatable Restraint (SIR) systems for automotive vehicles and the like, and, more specifically, to semiconductor integrated driver circuits which are employed in such automobile airbag systems for deploying airbags using igniters or squibs; and including a firing control section guaranteeing secure operation under any circumstances and also including circuit diagnostics for testing the proper operation capabilities of the drivers that supply the electrical energy to ignite the squibs.

(2) Description of the Prior Art

The main components of Supplemental Inflatable Restraint (SIR) systems for automotive vehicles and generally used as passenger protection systems in motor vehicles include an inflatable textile bag, named airbag, a propellant source (made e.g. from sodium azide pellets), an igniter or squib to initiate burning of the propellant source by means of a firing circuit driving said squib for causing inflation of the airbag. The squib is a detonator wire used for example to ignite the explosive charge that inflates the airbag in the automobile. The squib is a low resistance conductive wire with multiple coatings of an explosive material. At impact during an automobile accident, a large current flows through the squib, heats the wire, and ignites the explosive layers. This initial explosion sets off a secondary charge that inflates the airbag to protect the occupants. Alongside also necessary as another main component are a deployment circuit having at least one accelerometer as crash sensor, sensitive to vehicle motion, especially deceleration, and containing an electronic control module for determining when to deploy the airbag and sending a deployment pulse to the igniter, normally using a microprocessor system monitoring the accelerometer output for evaluating the severity of a crash to determine whether to deploy the airbag. The airbag, propellant, and igniter are by default contained in an airbag module (e.g., within a steering wheel for a driver airbag). The crash or safing sensor can be packaged separately or may be contained within the electronic control module.

This control module performs basic self-diagnostic monitoring of the SIR system each time the system is turned on (e.g., every time a vehicle is started). Any potential performance problems are identified and a warning light e.g. is illuminated on the

console, so that the automobile driver knows that the system needs to be serviced. The vehicle battery voltage or ignition system voltage empowering these deployment and firing circuits will, by the way, subsequently be called Airbag Voltage Supply (AVS) voltage. This voltage is generated from the battery supply and is present even in case of a battery disconnection, in order to safely supply the airbag system. The control circuit and the firing circuit are in general and to a large extent embodied with a specialized microprocessor system core on integrated circuit chips for the airbag deployment functionality, altogether called an Airbag Controller and Squib Driver. (In all currently known applications, the needed microprocessor is located on a different asic chip as the squib driver. 1st asic: processor and sensor interface; 2nd asic: squib driver together with diagnostics (and devices for power supply generation)). In any case an external harness leads to the squib at the site of the airbag, or in the case the vehicle is equipped with more airbags, this harness connects the squibs of each airbag to the squib driver chips. It is conceivable that eventually some portion of the harness might become damaged, i.e. short to ground (GND) or even to the AVS voltage. To forestall the possibility that such inadvertent electrical connection to the firing circuit might cause deployment of the airbag or disable the whole system, it is desirable to continuously monitor the system to detect any such event. It is common practice to perform diagnostic monitoring of the electrical connection of the squib elements, squib resistances, and electrical leakage or isolation in the squib circuits, among other tests. It is already known to diagnose a short of the firing circuit by feeding a small test current through the squib and through a biasing resistor to ground. The resulting bias voltage will depend on the current and if there are no shorts to the firing circuit the resulting test voltage will be at a prescribed

value. To assure this, the test current has to be carefully controlled. Where, for example, if the current is provided by a current source on an integrated circuit, the circuit must be trimmed during manufacture to assure the correct current output. Then the test voltage is sampled by an A/D converter e.g. and fed to the microprocessor where it is monitored to detect a low value indicative of shorting to ground or a high value indicative of shorting to supply voltage. Thus the monitoring circuit in the automobile continuously checks the squib resistance and reports values outside the acceptable range as a warning.

Preferred prior art circuits obeying to automotive industry regulations do not allow a direct galvanic connection of the squib to the supply voltages - neither to the AVS voltage nor to GND voltage with possible firing current flowing - during normal operation of the vehicle, i.e. not firing the squib, and therefore include two separate switches on every side of a squib. This means one high-side switch connects the squib to AVS voltage and another low-side switch connects the squib to GND voltage, thus the deployment of a squib is only initiated if these two independent switches of the firing loop are both closed; the firing loop formed by the vehicle battery between AVS and GND on one side and with said high-side switch, said squib to be fired and said low-side switch on the other side. Currently said squib driver switches are implemented using NPN, NMOS or DMOS transistors, which are controlled as switches by appropriate driver circuits. Due to supply voltage variations and deviations from the normal squib resistance from about 2 Ohms the current through the switches may vary between approximately 2A and 4.5A. For integrated squib power transistor switches however the

current flowing through these switching devices must be limited to approximately 3A, therefore it has to be measured and limited during said firing operation and additionally the transistors must be forced to reduce their on-resistance to avoid excessive power dissipation, which could lead to a premature destruction of said semiconductor switching devices. The current practice of sensing this current with resistors causes excess voltage drop that in consequence enlarges the unwanted power dissipation within the integrated power circuit. This disadvantage poses a major problem for that sort of circuits.

Another consequence of the aforementioned automotive industry requirements is the measurement of the isolation of the squib against AVS and GND, and also the determination of the squib resistance, which has to be performed during normal operation of the vehicle. Normal operation means that the squib is not firing. These measuring operations should be periodically performed by applying repeatedly cycling resistance measurements during normal operations of the vehicle. In one aspect, prior art solutions provide a method of testing a high-side driver and a low-side driver in an airbag squib circuit. The airbag squib circuit includes a squib element coupled between the high-side driver and the low-side driver. The high-side driver controllably provides a high-side voltage to one side of the squib element and the low-side driver controllably provides a low-side voltage to the other side of the squib element. Resistance of the squib element is tested for a resistance value laying within a predetermined resistance range. Current leakage associated with said squib element is tested to determine whether it is over a leakage threshold. An intermediate voltage from a weak power

supply is supplied to a test-point in the airbag squib circuit between the high-side driver and the low-side driver. One of the drivers is turned on while keeping the other one of the drivers off. Voltage at the test-point is continuously compared with a predetermined voltage range, which includes the intermediate voltage. This one driver is turned off in response to the voltage at the test-point being outside the predetermined voltage range, thereby detecting that this one driver is operating properly. If the voltage at the test-point remains in the predetermined voltage range for a predetermined time period, then this one driver is turned off and an indication is made that this one driver has failed.

Unless there is a failure, the other driver is then turned on while keeping the one driver off. A voltage at the test-point is continuously compared with the predetermined voltage range. The other driver is turned off in response to the voltage at the test-point being outside the predetermined voltage range, thereby detecting that the other driver is operating properly. If the voltage at the test-point remains in the predetermined voltage range for the predetermined time period, then the other driver is turned off and an indication is made that the other driver has failed.

In daily use of these circuits in vehicles and especially under all the existing environmental conditions appearing on earth during operation of an automobile another major problem is the degradation of the devices during lifetime and therefore a multitude of techniques and methods for their implementations has been specified in the past.

The main problem hereby is due to the fact, that in most cases the known prior art solutions are very elaborate and complicated when all the requirements as established by the automotive industry have to be met, thereby giving practical realizations leading to very costly devices.

It is therefore a challenge for the designer of such devices and circuits to achieve a high-quality and also low-cost solution. Several prior art inventions referring to such solutions describe related methods, devices and circuits, as well as technologies.

U. S. Patent 5,459,449 (to Ravas et al.) describes a method and an apparatus for diagnosing shorts in a SIR system, whereby airbags are deployed by firing circuits each containing a squib in series with a common control switch, and a control containing an accelerometer and a microprocessor for operating the switch to deploy the airbags. To diagnose shorts, a current source feeds a trickle current through each squib and a current limited voltage regulator across the switch passes the combined trickle currents to ground. The microprocessor senses the voltage across the switch via an A/D converter. That voltage goes low for a short to ground and high for a short to battery voltage.

U. S. Patent 5,675,242 (to Nakano) discloses a semiconductor integrated circuit in which a power field effect transistor (MOSFET) supplies a squib of automobile airbag systems with load current. The power MOSFET provides a squib with the load current; a load current signal which outputs from shunt resistor is provided to an operational amplifier consisting of multiple transistors with a negative feedback signal, so that the

load current to be supplied to the squib is restricted. The negative feedback operation is interrupted by a load current function interruption signal. A circuit, which consists of two current mirror circuits, composed of multiple transistors and a constant current source supplies the operational amplifier with constant current to interrupt the feedback operation.

U. S. Patent Application 2001/006309 (to Ueno et al.) shows an activating device for a vehicle passenger protection system in a vehicle, whereby an erroneous activating operation caused by improper operation of a microcomputer or electrical noise is prevented even though electronic switches are used to operate a squib. A microcomputer has output ports connected to first through third driving circuits controlling first through third electronic switching devices connected in series with a squib for deploying a passenger protection device. A timer circuit is connected to the first switching device by way of a prohibiting circuit provided as a hardware unit independent of the microcomputer.

Although these papers describe methods close to the field of the invention they differ in essential features from the method and especially the circuit introduced here.

SUMMARY OF THE INVENTION

A principal object of the present invention is to realize a very efficient driver device for the firing of igniters or squibs in form of very manufacturable integrated circuits at low cost.

Another principal object of the present invention is to provide an effective and secure method for operating said driver device for igniters or squibs implementable with the help of integrated circuits.

Also another principal object of the present invention is to always secure a controlled firing operation of the igniters or squibs by means of electronic switching devices with controlled current and voltage, i.e. with controlled energy.

Further a principal object of the present invention is to include a secure and continuous surveillance of the igniter or squib devices as well as the electronic switching devices and at the same time guaranteeing, that under no circumstances an unintentional firing operation can occur.

Also an object of the present invention is to include secure and reliable operating features into said driver device and at the same time to reach for a low-cost realization with modern integrated circuit technologies.

Further another object of the present invention is to economize the floor space of the chip layout needed for said switching devices, therefore using for the high-side switching device a single FET-switch, thus avoiding a large current mirror for high voltages normally consuming a rather large chip area.

Also further an object of the present invention is the inclusion of diagnostic test mechanisms into the circuit and its operation, which includes voltage, current and resistance measurements serving as surveillance of said electronic switches and said squib.

Another further object of the present invention is to combine needed current limitations and said onsite diagnostic tests in one operating function within said electronic switches by an implementation using current mirrors as control and/or switching devices.

Further another object of the present invention is to economize the floor space of the chip layout needed for said current mirrors.

Also another further object of the present invention is to avoid additional voltage drop due to said current measurement within said current mirror, thus avoiding additional power loss.

A further object of the present invention is the implementation of said current limiting regulation feature realized without control loop, thus avoiding possible instability of regulation loops.

Also an object of the present invention is thereby to establish an especially adapted method for said resistance measurement of said electronic switch as isolation measurement.

Also another object of the present invention is to resolve with said adapted method for said measuring of said electronic switch resistance also said resistance measurement of said squib.

A still further object of the present invention is to reduce the power consumption of the circuit by realizing inherent appropriate design features, such as trimming and limiting the maximum squib current to its absolutely necessary minimum for a secure firing operation.

Also an object of the invention is therefore to reduce the cost of the system by reducing the size of the external energy storing capacitor, made possible due to said current trimming and limiting.

Another further object of the present invention is to reduce the cost of manufacturing by implementing the circuit as a monolithic integrated circuit in low cost CMOS technology.

Another still further object of the present invention is to reduce cost by effectively minimizing the number of expensive components.

In accordance with the objects of this invention, a new method for the controlled operation and secure firing of igniters or squibs is described, capable of driving the necessary switching devices within a circuit branch connecting said squib via a high-side electronic switch to a power source and via a low-side electronic switch to circuit ground, incorporating separate power supply parts for high voltage and low voltage domains and equipped with elaborate intrinsic diagnostic and online testing features for circuit protection and operation securing purposes, altogether named Squib Driver circuit, comprising the following steps of providing a means for a Control and Test Unit for said Squib Driver circuit, containing a Firing Control (FC) unit and a Diagnostic and Online Test (DOT) unit with input and output connections for - inter alia - an electrical Safing Sensor, a Fuel Cut-Off During Collision operation and a Diagnostic Lamp Driver signal, and further additionally containing measuring or sensing input signals and control output signals; providing for said Squib Driver circuit means for connecting an external main power supply via a mechanical Safing Sensor and means for connecting to ground; providing for said Squib Driver circuit external means for said power supply using a single charge pump circuit for storing said main supply energy within an external

storage capacitor as so called AVS voltage; providing for said Squib Driver circuit connection means for connecting an external igniter device or squib to a first connection pin named high-side connection and to a second connection pin named low-side connection; providing a first internal means for switching operations of said external igniter device or squib on its high-side connection point, named high-side switching device; providing a second internal means for switching operations of said external igniter device or squib on its low-side connection point, named low-side switching device; providing a first internal means for driving said internal high-side switching device, named High-Side Driver (HSD) circuit; providing other internal means for supplying multiple driver currents to said internal low-side switching device using controllable and switchable current source circuits; providing means for connection of said measuring or sensing input signals from said high-side and low-side switching devices to said Control and Test Unit; providing means for connection of said control output signals from said Control and Test Unit to said controllable and switchable current source circuits for said low-side switching device; implementing said high-side switching device as a single NMOS FET switch transistor, thus economizing chip space otherwise needed for implementing more complex structures for higher voltages; implementing said low-side switching device with the help of a pair of NMOS transistors in current mirror configuration; implementing said high-side switch driver circuit with the help of an integrated HSD circuit, consisting of two anti-phased driven current mirror differential switching amplifier NMOS&PMOS stages each with PMOS output booster circuit and both driving one PMOS output driver stage biased by an internal current source; implementing for said low-side switching device said controlled pair of

switchable current sources as drivers, whereby the one current source defines the normal diagnostic and test operations and the other current source the firing operation; initiating a Basic Function Test Cycle for said Squib Driver circuit during power on of said Squib Driver circuit, testing regular functionality of said internal driver circuits and switches and said external igniter device or squib; starting, in normal operation mode, the Diagnostic and Test Cycle for continuous surveillance of prescribed isolation and resistance values i.e. of the regular functioning of the system; testing for isolation values of the high-side and low-side switching devices versus supply voltage and ground; measuring appropriate test voltages at the squib and said high-side and low-side switching devices in the switched squib branch with the help of given diagnostic currents; calculating the resistance of the squib and said high-side and low-side switching devices in the switched squib branch; evaluating said measured and calculated values and compare to the prescribed and for a regular operation required and defined values; activating in case of failure an alarming signal; calculating with the help of said voltage and resistance values secure firing current values for said high-side and said low-side switching devices, thus trimming, i.e. setting-up said controlled driving currents to their operational necessary minimum, and thus limiting said main supply energy stored within said external storage capacitor to an optimum; continuing the Diagnostic and Test Cycle from its starting point above during normal operation of the Squib Driver circuit; and firing the squib in case of emergency by switching on at the same time, both the high-side and the low-side switching devices and whilst observing given current limitations with the help of said controlled driving currents.

Further in accordance with the objects of this invention, a circuit, implementing said new method is achieved, capable of realizing a driver device for secure and reliable firing of an igniter or squib, connecting said squib via a high-side electronic switch to a power source and via a low-side electronic switch to circuit ground, incorporating separate power supply parts for high voltage and low voltage domains and equipped with elaborate intrinsic diagnostic and online testing features for circuit protection and operation securing purposes, comprising the following means: a means for control of said firing, said diagnostic and said online testing; a means for said high-side switching of said squib to said power source; a means for said low-side switching of said squib to said circuit ground; a means for said high voltage domain power supply; a means for said low voltage domain power supply; a means for secured supply of electrical energy to said means for said high-side switching derived from said high voltage domain; a means for secured supply of electrical energy to said means for said low-side switching derived from said low voltage domain; a means for driving said high-side switching means for said squib controlled by said means for control of firing, diagnostic and online testing and supplying drive current to said high-side switching means either for the case of said diagnostic and online testing operations or for the case of said firing operation; and a means for connecting said high-side switching means and said low-side switching means to said means for control of firing, diagnostic and online testing in order to execute said diagnostic measurement and online testing whereby in said case of diagnostic and online testing operations a switchable and controllable current flow is initiated in conjunction with appropriate voltage measurements and resistance evaluations thereby strictly observing that no firing condition for said squib are allowed

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to occur and whereby in said case of firing operation a secure firing of said squib is always guaranteed.

BRIEF DESCRIPTION OF THE DRAWINGS

In the accompanying drawings forming a material part of this description, the details of the invention are shown:

FIG. 1 shows the essential components for the preferred embodiment of the present invention i.e. a circuit diagram of the complete squib driver arrangement. The circuit diagram illustrates the essential circuit blocks – among other things the firing control and diagnostic testing circuit, High-Side Driver (HSD), the switch FETs and the squib - and their interconnections, all realizable with a variety of modern monolithic integrated-circuit technologies.

FIG. 2 depicts in form of a circuit schematic an exemplary realization of the integrated HSD circuit within the implementation of the invention according to FIG. 1.

FIGS. 3A - 3D describe with the help of a flow diagram the method for operating a squib driver implemented with an electrical circuit as shown in FIGS. 1 & 2 for example.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

The preferred embodiments disclose a novel optimized circuit conception for a squib driver using modern integrated digital circuits and an exemplary circuit thereto.

The description of the preferred embodiments of the invention is subdivided into two parts; first an overall description of the whole implementation and its conceptional design is given and second a detailed description of an incorporated driver circuit part is presented, which is called High-Side Driver (HSD) and forming an essential part of the invention.

The approach for driving squibs within SIR systems implemented here is to some extent already known and has therefore been described in detail in the prior art description section above. Its in-depth comprehension is indeed a prerequisite for the understanding of the following new circuit approaches and design principles.

Important and valid are the respective automotive industry regulations, which do not allow during normal operation of the vehicle for a direct galvanic connection of the squib to either of the both voltages - neither to the Airbag Voltage Supply (AVS) voltage nor to GND voltage - or a closed FET switch contacting at the same time of both low resistance switches together; normal operation signifying thereby not firing the squib. Therefore standard design includes two separate switches on every side of a squib in a

"vice-versa locking" operation mode, which is also effective in every possible testing situation. This means one high-side switch connects the squib to AVS voltage and another low-side switch connects the squib to GND voltage, thus the deployment of a squib is only initiated if these two independent switches of the firing loop are closed; the firing loop formed by the vehicle battery between AVS and GND on one side and with said high-side switch, said squib to be fired and said low-side switch on the other side.

Currently said squib driver switches are implemented using NPN, NMOS or DMOS transistors, which are controlled as semiconductor switches by appropriate driver circuits. Due to variations in the squib resistance from normally about 2 Ohms and the drain-source-on resistance of the two needed switches, the current through the switches may vary between approximately 1.5A and 4.5A. For integrated squib power transistor switches the current flowing through these semiconductor switching devices must be limited to approximately 3A, and by reducing this current to a safe but nevertheless reliable minimum with respect to firing the squib, the needed external energy storage capacitance C_{store} can also be reduced in size, which is very important for economizing the overall system costs. Therefore this current has to be measured and controlled during said firing operation and the transistors must be forced to reduce their on-resistance to avoid excessive power dissipation, which could lead to a premature destruction of said switching devices. The current practice of sensing this current with resistors causes an additional voltage drop, which in consequence enlarges the unwanted power dissipation within the integrated power circuit. This disadvantage poses a major problem for these sorts of circuits.

Another important consequence of the aforementioned requirements by the automotive industry is a virtually incessant measuring of the isolation of the squib against AVS and GND, and also a quasi permanent determination of the squib resistance, which has to be performed during normal operation of the vehicle and can be appropriately solved by using periodically cycling measurement methods. Occurring faults can therefore be recognized almost immediately and will be signaled to the operator and/or be processed adequately by the security system of the vehicle. When performing electrical testing involving the squibs, care must be taken to avoid application of any current to a squib that could cause an inadvertent deployment of the airbag. Due to the cost of replacing an airbag module and the loss of supplemental protection until replacement occurs, diagnostic monitoring should not increase the chances of an inadvertent deployment. Therefore a very desirable test to be able to perform is a driver circuit test in which a squib driver circuit can be activated in a test mode without igniting the squib. Such a test has to verify that said semiconductor switches in series with the squib element itself would conduct as intended during an actual deployment event. However, such a test is problematic since the activation of each of these switches partially completes the deployment circuit. If certain other faults exist, or if the switch activation is not implemented properly, unintended deployments could occur. In a squib activating driver device for a passenger protection system in a vehicle an erroneous activating operation caused by improper operation of a microprocessor or any other component - or caused even by electrical noise - has to be prevented although electronic semiconductor switches are used to operate the squib.

Referring now to FIG. 1, the preferred embodiment of the circuit diagram implementing the complete squib driver arrangement of the present invention is illustrated. The essential functional components comprise the Firing Control **120** (FC) and Diagnostic & Online Testing **150** (DOT) circuit within control and test unit **100**, all the input, output and ground pins of the circuit (items **200** ... **290**), the igniter or squib (item **900**), diverse current sources for driver switch diagnostics and firing I_1 , I_2 and I_3 (items **320**, **325**, **310**), I_1 and I_2 thereby controlled via control signal lines (items **117** and **119**), one high-side driver NMOS-FET N_{30} switch (item **410**) for squib **900** and driven by a High-Side Driver (HSD, item **500**) device, and two low-side driver NMOS-FETs N_{10} and N_{20} (items **420** and **425**) in current mirror configuration and serving as low-side driver switch for squib **900**. Also depicted are several external power supplying components being inputs from charge pumps (items **710**, **720**) or being the extra energy storing capacitor C_{store} (item **850**) serving as storage load for said charge pump **720** whereby the charge pump voltage V_{cpAVS} (for item **720**) as seen over C_{store} (**850**) is always the main power supply source of the airbag application. This extra energy storage is especially of importance through its boosting and buffering in an emergency case, when the battery of the vehicle is not working any more i.e. not delivering enough power for secure ignition of the squib in case of an accident. Also shown is the power input voltage V_{Bat} via connector from the vehicle battery **800** together with its reverse battery protection diode **810**, whereby this voltage V_{Bat} is initially charging said capacitor C_{store} (**850**) during the power-up sequence. After this the charge pump **720** is charging this connection node **820** (diode **810** – capacitor **850**) up to a voltage of 15-25V and

thus disconnecting V_{Bat} by said diode **810** from said node **820**, now delivering the Airbag Voltage Supply (AVS) voltage. That means that the power source Airbag Voltage Supply (AVS) for the driver circuit is independent from the battery of the car, where V_{Bat} (**800**) is the battery voltage. The charge-pump-AVS output node (**720**) delivers 15-25V for power supply, this voltage is named V_{cpAVS} . This node is also charging C_{store} (**850**) and C_{store} is delivering the energy for firing the squib. The node charge-pump-Gate (**710**) requires the voltage V_{cpG} , with a voltage of additional 5V higher than V_{cpAVS} , in order to deliver the needed voltage to the gate of the transistor N_{30} (**410**). Summarizing this: in the high voltage domain the voltage V_{cpAVS} (**720**) is generated out of the battery voltage V_{Bat} (**800**) and thus establishing the power source AVS for the airbag system. Out of V_{cpAVS} (**720**), the following supplies are generated: voltage V_{cpG} for charge-pump-Gate node (**710**), which is 5V higher as V_{cpAVS} and thus also in the high voltage domain and a separate 5V supply at node (**700**), delivering power to the low voltage domain. Further shown in FIG. 1 are the safing sensor components for either electrical **600** (input pin **240**) or mechanical type (items **620**, **630** and **640**) devices.

Summarizing the essential operational features of the circuit we find, that the squib driver circuit contains a high-side FET switch N_{30} (**410**) which connects one connector pin of the squib (**900**) via the safing sensor to the Airbag Voltage Supply (V_{cpAVS} ; **720**) and a low side switch N_{10} (**420**) which connects the second connector pin of the squib (**900**) to GND (**200**). The two ground nodes GND and AGND are separated because a large current will run when the squib is fired. This causes a big voltage shift, which could the lead, the sensor side circuits as well as the digital circuitry to

malfunctions. The ground nodes are connected together outside of the package, which makes the internal AGND stable. The regular resistance value of the squib (900) is about 2 Ohm. At normal operation of the vehicle (i.e. not firing the squib) the squib is not allowed to have a connection neither to V_{cpAVS} (720) nor to GND (200). Therefore regularly measuring during normal operation the isolation values of the squib (900) vs. V_{cpAVS} (720) and vs. GND (200) is a requirement. The healthy condition of the squib (900) is additionally supervised by regularly measuring the resistance of the squib (900). The diagnostic current values during these diagnostic measurements must be limited to currents lying in the range of 50mA sufficiently far away from the values of the firing current. The current value for firing the squib (900) must be supplied with values between 2A and about 3A. Having the squib fired by said low-side current mirror N_{10} - N_{20} (420-425; operating as a closing FET switch) and said high-side FET switch N_{30} (410) closed, all operating in the AVS voltage (15-25V; (max.40V; i.e. able to tolerate a 40V rise at load dump)) domain, all the diagnostic operations for these FET switches (410 and 420-425) and for the squib (900) can be controlled and measured by control signals completely derived from the 5V (or 3.3V) low-voltage domain, only the squib branch being supplied from the AVS high-voltage domain; thus easily fulfilling the operating demands established by security requirements.

Still with the help of FIG. 1 looking now somewhat closer to the diagnostic functions of the circuit of the invention during normal operation, we find that in diagnostic mode for the squib (900), which is controlled by the DOT circuit block (150), the squib (900) is powered by the AVS voltage V_{cpAVS} (720) with a maximum current

limited to 50mA. The voltage sensing signals measured are V_1 , V_2 , V_3 , and V_4 fed into the DOT (150) circuit by lines 112, 115, 114 and 111, referenced to GND 110. Switching on the switch FET N_{30} (410) with a limited current from the source I_3 (310), the two voltages V_1 (112) and V_2 (115), and thus the voltage drop V_1/V_2 can be measured. With this a short to GND can be detected. In case of a short the squib (900) cannot be fired because the measurement current is limited and too small for firing the squib (900). Switching on the current mirror FET N_{10} (425) with a limited current from the source I_2 (325), the voltage drop V_3/V_4 (114/111) can be measured. With this a short to AVS can be detected. In case of a short, again the squib (900) cannot be fired because the measurement current is limited and too small for firing the squib (900). Activating the current source FET N_{10} (420) and the switch FET N_{30} (410), the voltage drop V_2/V_3 (115/114) of the squib and the serial resistance of the squib can be measured. With 50mA into 2 Ohms we have a 100mV voltage drop for a working squib. The current is however limited to 50mA by the current source (310), so in the last case maximally 50mA are running over the squib.

Describing now the safing operation of the circuit of the invention - i.e. firing the squib (900) - implies that current source I_1 (325) controlled by the firing control signal (117) from circuit block FC (120) injects a defined current to the current mirror N_{10} - N_{20} (420-425). So N_{10} (420) will connect the lower side of the squib (900) to GND unless the current exceeds the maximum mirrored current. The high-side switch N_{30} (410) is controlled via the HSD (500) device shown, which is described later with the help of FIG. 2. The gate of transistor N_{30} (410) is forced to raise its potential 5V higher than

V_{cpAVS} by an additional charge pump, as described above and located in the power generations block which is not described in this invention.

In case of emergency during a car accident, i.e. when the battery of the vehicle may be already out of order, the energy already pumped by said charge pump into capacitor C_{store} (850) during normal operations and stored within said capacitor as AVS voltage V_{cpAVS} has to be sufficient for said firing of the squib (900) and to supply the needed driver circuit parts with energy for the triggering during said safing operation, whereby the capacitor C_{store} (850) is a very expensive part of the airbag system. By trimming the maximum current through the squib, thus obtaining a reduction of the current to a safe minimum, the capacitor can be reduced in value to save cost. Said trimming and limiting of the maximum squib current therefore helps for a low-cost solution: the capacitance value of capacitor C_{store} (850) can be kept as small as possible, thus allowing to assemble the system with cheaper capacitor components, saving production costs.

Referring now to the circuit schematic of FIG. 2 an exemplary realization of the integrated HSD (500) circuit controlling MOSFET N_{30} (410) within the implementation of the invention according to FIG. 1 is described in some detail. Essentially included are multiple FET transistors of NMOS type (N_1 to N_7), multiple FET transistors of PMOS type (P_1 to P_{10}), a digital inverter circuit (INV) for the digital input signal **DigInp**, a current source **I** and some additional integrated resistors $R_1 \dots R_4$. The external connection pins are used as input for signal **DigInp**, connections to supply voltages

V_{bias} , V_{cpG} and GND and the output connections for node signals N_{drive} and N_{sense} . The high-side MOSFET switch e.g. N_{30} (item 410 from FIG. 1; here shown dashed) is controlled via said driver device HSD (500) as shown, via said connection nodes and lines (also drawn dashed) and designated N_{drive} and N_{sense} . Both transistors P_1 and P_2 are controlled the same way, so only the functioning of one control circuit is described; (N_2 , N_3 , N_4 , P_3 , P_4 , P_5 , P_6 , R_1 , R_2 have the same function as N_1 , N_5 , N_6 , P_7 , P_8 , P_9 , P_{10} , R_3 , R_4). The differential pair of transistors N_3 - N_4 that is used as a switch (current steering) is switching the current generated by N_2 either to transistor P_5 that acts as a diode or to transistor P_6 . If the current is steered through N_3 , the gate-source voltage at P_5 induces a current at transistor P_3 . Because N_4 carries no current the gate of P_4 reaches the voltage of node N_{drive} , consequently transistor P_4 becomes non-conductive. This forces transistor P_1 to be also non-conductive. The nodes N_{drive} and N_{sense} are thus high impedance connected. Having transistor N_4 conductive, N_3 delivers no current and there is no current mirrored via P_5 to P_6 and also not to P_3 . The current through N_4 causes a voltage drop over resistor R_2 , connecting to the gate of P_4 . This gate of P_4 , which is connected to this node, opens then transistor P_4 and forces a current rise through resistor R_1 until the gate-source voltage of P_4 is limiting the current, thus generating a constant voltage, which switches on P_1 . The current source I_1 serves to compensate for the process and temperature dependencies of P_4 to get a stable voltage of 5V over R_1 . P_1 shorts the gate-source ($N_{drive} - N_{sense}$) of transistor N_{30} that gets N_{30} into high impedance state. At this moment transistor N_7 is conductive to ensure that the voltage potential at node N_{drive} is always following the voltage potential at N_{sense} . The very same control functions are used to control the comparable transistor P_2 . A

transistor with a function like N_7 is not necessitated because the supply voltage for this comparable structure is always connected to V_{cpG} . For an integrated circuits realization of this structure preferably a symmetrical NMOS or a symmetrical DMOS process technology is needed.

Referring now to FIGS. **3A - 3D**, the method for operating a squib driver circuit implemented using electrical circuit schematics as shown for example in FIGS. **1 & 2** is described in some detail with the help of a flow diagram for every essential step.

Steps **502** to **516** list all the necessary means for the implementation of said method, whereby the first step **502** provides a means for a Control and Test Unit for a Squib Driver circuit, containing a Firing Control (FC) unit and a Diagnostic and Online Test (DOT) unit with input and output connections for - inter alia - an electrical Safing Sensor, a Fuel Cut-Off During Collision operation and a Diagnostic Lamp Driver signal, and further additionally containing measuring or sensing input signals and control output signals and step **504** provides for said Squib Driver circuit means for connecting an external main power supply via a mechanical Safing Sensor and means for connecting to ground, in step **505** for said Squib Driver circuit external means are provided for said power supply using a single charge pump circuit for storing said main supply energy within an external storage capacitor as AVS voltage. Step **507** further provides for said Squib Driver circuit connection means for connecting an external igniter device or squib to a first connection pin named high-side connection and to a second connection pin named low-side connection and steps **510** and **511** provide a first internal means for

switching operations of said external igniter device or squib on its high-side connection point, named high-side switching device and a second internal means for switching operations of said external igniter device or squib on its low-side connection point, named low-side switching device. With step **512** and step **513** another internal means for driving said internal high-side switching device, named High-Side Driver (HSD) circuit and again another internal means for supplying multiple driver currents to said internal low-side switching device using controllable and switchable current source circuits are provided. Step **515** provides means for connecting of said measuring or sensing input signals from said high-side and low-side switching devices to said Control and Test Unit and finally step **516** provides means for connecting of said control output signals from said Control and Test Unit to said controllable and switchable current source circuits for said low-side switching device.

Starting with step **520** the implementation of said high-side switching device as a single NMOS FET switch transistor is described, in step **521** implementing said low-side switching device with the help of a pair of NMOS transistors in current mirror configuration follows, together with step **523** implementing said high-side switch driver circuit with the help of an integrated HSD circuit, consisting of two anti-phased driven current mirror differential switching amplifier NMOS&PMOS stages each with PMOS output booster circuit and both driving one PMOS output driver stage biased by an internal current source. Step **526** implements for said low-side switching device said controlled pair of switchable current sources as drivers, whereby the one current source

defines the normal diagnostic and test operations and the other current source the firing operation.

In step **530** the normal operation of the circuit begins by initiating a Basic Function Test Cycle for said Squib Driver circuit during power on of said Squib Driver circuit, testing regular functionality of said internal driver circuits and switches and said external igniter device or squib, and step **540** starts, still in normal operation mode, the Diagnostic and Test Cycle for continuous surveillance of prescribed isolation and resistance values i.e. of the regular functioning of the system. With step **542** a test for isolation values of the high-side and low-side switching devices versus supply voltage and ground is made, then step **544** measures appropriate test voltages at the squib and said high-side and low-side switching devices in the switched squib branch with the help of given diagnostic currents, step **550** then calculates the resistance of the squib and said high-side and low-side switching devices in the switched squib branch, and in step **552** the evaluation of said measured and calculated values and comparison to the prescribed and for a regular operation required and defined values is made, activating in case of failure an alarming signal at step **560**, all these are steps in normal operation mode. Another normal mode step **570** calculates with the help of said voltage and resistance values secure firing current values for said high-side and low-side switching devices, thus trimming, i.e. setting-up said controlled driving currents to their operational necessary minimum, and thus limiting said main supply energy stored within said external storage capacitor to an optimum and so continuing the Diagnostic and Test Cycle from its starting point above during normal operation of the Squib Driver circuit

during step **580**. Normal operation ends with step **590**, firing the squib in case of emergency by switching on, both the high-side and the low-side switching devices at the same time and whilst observing given current limitations with the help of said controlled driving currents.

As shown in the preferred embodiments and evaluated by circuit analysis, the novel circuits and methods provide an effective and manufacturable alternative to the prior art.

While the invention has been particularly shown and described with reference to the preferred embodiments thereof, it will be understood by those skilled in the art that various changes in form and details may be made without departing from the spirit and scope of the invention.

What is claimed is: